

MICROCOPY RESOLUTION TEST CHART
NATIONAL BUREAU OF STANDARDS-1963-A

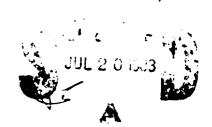
RADC-TR-83-96 In-House Report April 1983



A PROOF OF THE ODD-SYMMETRY OF THE PHASES FOR MINIMUM WEIGHT PERTURBATION, PHASE-ONLY NULL SYNTHESIS

Robert A. Shore

APPROVED FOR PUBLIC RELEASE; DISTRIBUTION UNLIMITED



ROME AIR DEVELOPMENT CENTER Air Force Systems Command Griffiss Air Force Base, NY 13441

MIC FILE COP

This report has been reviewed by the RADC Public Affairs Office (PA) and is releasable to the National Technical Information Service (NTIS). At NTIS it will be releasable to the general public, including foreign nations.

RADC-TR-83-96 has been reviewed and is approved for publication.

APPROVED: Thepp Blacksmi

PHILIPP BLACKSMITH

Chief, EM Techniques Branch

Electromagnetic Sciences Division

APPROVED: Welan Chleel

ALLAN C. SCHELL

Chief, Electromagnetic Sciences Division

FOR THE COMMANDER: Sohn P. Kins

JOHN P. HUSS

Acting Chief, Plans Office

If your address has changed or if you wish to be removed from the RADC mailing list, or if the addressee is no longer employed by your organization, please notify RADC (EECS) Hanscom AFB MA 01731. This will assist us in maintaining a current mailing list.

Do not return copies of this report unless contractual obligations or notices on a specific document requires that it be returned.

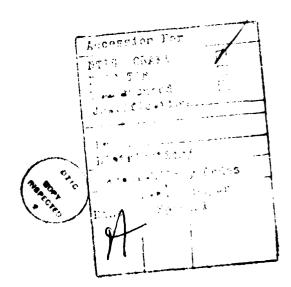
Unclassified
SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

REPORT DOCUMENTATION PAGE	READ INSTRUCTIONS BEFORE COMPLETING FORM	
1 REPORT NUMBER 2. GOVT ACCESSION NO.	3 RECIPIENT'S CATALOG NUMBER	
RADC-TR-83-96 AD-4/30	+ · · · · · · · · · · · · · · · · · · ·	
4 TITLE (and Subtitle)	5. TYPE OF REPORT & PERIOD COVERED	
A PROOF OF THE ODD-SYMMETRY OF THE PHASES FOR MINIMUM WEIGHT PERTURBA-	In-House	
TION, PHASE-ONLY NULL SYNTHESIS	6 PERFORMING ORG. REPORT NUMBER	
7 AUTHOR(s)	8 CONTRACT OR GRANT NUMBER(s)	
Robert A. Shore		
9 PERFORMING OPPORTUNITY NAME AND ADDRESS Rome Air Development Center (EECS)	10 PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS	
Hanscom AFB	61102F	
Massachusetts 01731	2305J304	
11 CONTROLLING OFFICE NAME AND ADDRESS	12 REPORT DATE	
Rome Air Development Center (EECS)	April 1983	
Hanscom AFB	13 NUMBER OF PAGES	
Massachusetts 01731	20	
14 MONITORING AGENCY NAME & ADDRESS(if different from Controlling Office)	15 SECURITY CLASS (of this report)	
	Unclassified	
	154 DECLASSIFICATION DOWNGRADING SCHEDULE	
15. DISTRIBUTION STATEMENT (a) this Report;	<u> </u>	
Assumed for public value as distribution unlimited		
Approved for publice release; distribution unlimited.		
17 DISTRIBUTION STATEMENT of the abstract entered in Black 20, if different from Report)		
18 SUPPLEMENTARY NOTES		
the state of the s		
19 KEY WORDS (Continue on reverse side if necessary and identify by block number)		
Phase-only control		
Null synthesis		
Linear array antennas		
Symmetry		
Optimization 20 ABSTRACT (Continue on reverse side if necessary and identity by block number)		
A proof is given of the odd-symmetry property of the phase perturbations		
required to impose nulls in a real linear array antenna pattern using phase- only weight control subject to minimization of the absolute weight perturba-		
Lanti dealght control subject to mainimization or the		
tions. The perturbed weights are, therefore, con respect to a phase reference at the center of the a	ijugate symmetric with	

SECURITY CLASSIFICATION OF THIS PAGE(When Data Entered)	

Preface

The author wishes to express his thanks and appreciation to Dr. Ronald L. Fante for a very helpful communication, to Dr. Hans Steyskal for many stimulating conversations on the subject of this report, and to Dr. Robert J. Papa for a critical reading of the draft of this report.



Contents 1. INTRODUCTION 7 2. PROOF OF THE ODD-SYMMETRY OF THE PHASES FOR MINIMUM WEIGHT PERTURBATION, PHASE-ONLY NULL SYNTHESIS 8 3. CONCLUDING REMARKS

19

REFERENCES

A Proof of the Odd-Symmetry of the Phases for Minimum Weight Perturbation, Phase-Only Null Synthesis

1. INTRODUCTION

The current interest in phase-only control of the element weights of linear arrays for adaptive nulling 1-9 and null synthesis 10-16 is a result of the increasing importance of phased arrays and adaptive processing. Null synthesis has considerable value for adaptive nulling in that it can help determine limits to what can be achieved adaptively.

In null synthesis, as in adaptive nulling, it is generally undesirable to impose nulls in a given array antenna pattern at the expense of large distortion in regions of the pattern aside from the imposed null locations. One way to reduce such pattern distortion is to minimize the perturbations of the element weights. The imposing of nulls in the pattern of a linear array by phase-only weight control subject to minimization of the weight perturbations is, unlike for combined phase and amplitude control, a nonlinear problem and, in general, cannot be solved analytically. Numerical techniques 14, 17 must be used to calculate the phases required for minimized weight perturbation, phase-only null synthesis.

If the pattern in which nulls are to be imposed is real, it is reasonable to assume that the pattern satisfying the null constraints and corresponding to minimum element weight perturbations should likewise be real. The phase perturbations of

⁽Received for publication 11 April 1983)

Because of the large number of references cited above, they will not be listed here. See References, page 19.

the element weights are then odd-symmetric with respect to a phase reference located at the center of the array. If nonlinear programming or other numerical techniques are used to calculate the phases for null synthesis, the odd-symmetry property of the phases can be used to reduce the number of unknown phases by a factor of a half, thereby significantly increasing computational efficiency. Although intuitively reasonable, nevertheless a proof of the odd-symmetry property is desirable. In an earlier report, ¹⁸ the author proved the odd-symmetry property for the case of a single imposed null. The method of proof, however, unfortunately did not generalize to multiple imposed nulls. It is the purpose of this report to give a general proof of the odd-symmetry property.

2. PROOF OF THE ODD-SYMMETRY OF THE PHASES FOR MINIMUM WEIGHT PERTURBATION, PHASE-ONLY NULL SYNTHESIS

We consider a linear array of N equispaced isotropic elements whose field pattern is given by

$$p_0(u) = \sum_{n=1}^{N} a_n e^{jd_n u}$$
 (1)

In Eq. (1) the $\{a_n\}$ are the complex element weights,

$$d_n = (N-1)/2 - (n-1) = -d_{N-n+1}$$
, $n = 1, 2, ..., N$ (2)

and

 $u = 2\pi/\lambda d \sin \theta$.

where

 $\lambda = wavelength$

d = interelement spacing, and

 θ = angle measured from broadside to the array.

The phase reference is taken to be the center of the array. The pattern is assumed real so that the complex element weights satisfy the relation 10

^{18.} Shore, R.A. (1983) On the Odd-Symmetry of Minimum Phase-Only Perturbations, RADC-TR-83-26.

^{19.} Oppenheim, A.V., and Schafer, R.W. (1975) <u>Digital Signal Processing</u>, Prentice-Hall, N.J., pp. 24-26.

$$a_{N-n+1} = a_n^*$$
 , $n = 1, 2, ..., N$. (3)

Let ϕ_n , $n=1, 2, \ldots$, N be the set of phase perturbations that (a) imposes nulls in the pattern at the locations $u=u_k$, $k=1, 2, \ldots$, K:

$$\sum_{n=1}^{n} a_{n} e^{j\phi_{n}} e^{jd_{n}u_{k}} = 0 , k = 1, 2, ..., K$$
(4)

and (b) minimizes the weighted sum of the squares of the absolute values of the element weight perturbations

$$F = \sum_{n=1}^{N} c_n \left| a_n \left(e^{j\phi_n} - 1 \right) \right|^2 . \tag{5}$$

The weighting coefficients, $\{c_n\}$, in Eq. (5) are assumed real, positive, and symmetric:

$$c_{N-n+1} = c_n$$
 , $n = 1, 2, ..., N$. (6)

We wish to show that the phase perturbations are odd-symmetric:

$$\phi_{N-n+1} = -\phi_n$$
 , $n = 1, 2, ..., N$, (7)

so that the perturbed pattern,

$$p(\mathbf{u}) = \sum_{n=1}^{N} \mathbf{a}_{n} e^{\mathbf{j} \phi_{n}} e^{\mathbf{j} d_{n} \mathbf{u}}$$

is real.

The choice of $c_n = 1$ for all n makes F the sum of the squares of the absolute values of the weight perturbations. For half wavelength spacing of the array elements, this is equivalent to minimizing the mean square pattern perturbation for 9 from $-\pi/2$ to $+\pi/2$. Other choices of the c_n with practical application to null synthesis are also possible: $\frac{1}{2}$ for example, $\frac{1}{2}$ and $\frac{1}{2}$.

The proof of Eq. (7) uses the method of Lagrangian multipliers. 20 We first rewrite the null constraints of Eq. (4) in the form

$$\sum_{n=1}^{N} a_{n} \left(e^{j\phi_{n}} - 1 \right) e^{jd_{n}u_{k}} = -p_{o}(u_{k}) , \quad k = 1, 2, ..., K$$
 (8)

and then make the constraints purely real by multiplying the left-hand side of Eq. (8) by its complex conjugate and squaring the (real) right-hand side, thus obtaining

$$\sum_{n=1}^{N} \sum_{m=1}^{N} a_n a_m^* \begin{pmatrix} j \phi_n - 1 \end{pmatrix} \begin{pmatrix} e^{-j \phi_m} - 1 \end{pmatrix} e^{j(d_n - d_m)u_k} - p_0^2(u_k) = 0 ,$$

$$k = 1, 2, ..., K .$$
(9)

Since

$$F = \sum_{n=1}^{N} c_n |a_n|^2 (e^{j\phi_n} - 1) (e^{-j\phi_n} - 1)$$

$$= \sum_{n=1}^{N} c_n |a_n|^2 (2 - 2\cos\phi_n)$$

$$= 2 \sum_{n=1}^{N} c_n |a_n|^2 - 2 \sum_{n=1}^{N} c_n |a_n|^2 \cos \phi_n , \qquad (10)$$

minimizing F is equivalent to maximizing

$$F' = \sum_{n=1}^{N} c_n |a_n|^2 \cos \phi_n . {(11)}$$

Fletcher, R. (1981) <u>Practical Methods of Optimization</u>; Vol. 2, <u>Constrained Optimization</u>, John Wiley & Sons, New York, Ch. 9.

We now form the Lagrangian

$$L = F' + \sum_{k=1}^{K} \lambda_k C_k$$

where the constraint functions, $C_{\mathbf{k}}$, from Eq. (9) are given by

$$C_{k} = \sum_{n=1}^{N} \sum_{m=1}^{N} a_{n} a_{m}^{*} \left(e^{j\phi_{n}} - 1 \right) \left(e^{-j\phi_{m}} - 1 \right) e^{j(d_{n} - d_{m})u_{k}} - p_{o}^{2}(u_{k}) , \quad (12)$$

and the $\{\lambda_k\}$ are the (real) Lagrangian multipliers. For the $\{\phi_n\}$ to locally maximize (or minimize) F' subject to satisfying the constraints $C_k=0$ it is necessary that the gradient of L with respect to the $\{\phi_n\}$ be zero. Accordingly we differentiate L with respect to an arbitrary one of the $\{\phi_n\}$, say ϕ_p , and equate the derivative to zero:

$$\frac{\partial \mathbf{F'}}{\partial \phi_{\mathbf{p}}} = -\sum_{\mathbf{k}=1}^{K} \lambda_{\mathbf{k}} \frac{\partial \mathbf{C}_{\mathbf{k}}}{\partial \phi_{\mathbf{p}}} . \tag{13}$$

From Eq. (11)

$$\frac{\partial F'}{\partial \phi_p} = -c_p |a_p|^2 \sin \phi_p . \qquad (14)$$

To differentiate C_k with respect to ϕ_p we group the terms of the double summation in Eq. (12) containing ϕ_p according as to whether (1) n = p, $m \neq p$; (2) $n \neq p$, m = p, or (3) n = m = p. For the first group of terms

$$\frac{\partial}{\partial \phi_{p}} \left[a_{p} \left(e^{j\phi_{p}} - 1 \right) e^{jd_{p}u_{k}} \sum_{\substack{m=1 \ m \neq p}}^{N} a_{m}^{*} \left(e^{-j\phi_{m}} - 1 \right) e^{-jd_{m}u_{k}} \right]$$

$$= j a_{p} e^{j\phi_{p} \int_{0}^{jd} p^{u_{k}}} \left[\sum_{m=1}^{N} a_{m}^{*} \left(e^{-j\phi_{m}} - 1 \right) e^{-jd_{m}u_{k}} - a_{p}^{*} \left(e^{-j\phi_{p}} - 1 \right) e^{-jd_{p}u_{k}} \right]$$

$$= -j p_0(u_k) a_p e^{j(\phi_p + d_p u_k)} - j |a_p|^2 (1 - e^{j\phi_p}) , \qquad (15a)$$

where we have used Eq. (8) and the fact that $p_0(u)$ is real. The contribution of the second group of terms to $\frac{\partial C_k}{\partial \phi_p}$ is simply the complex conjugate of that of the first group

$$j p_{o}(u_{k}) a_{p}^{*} e^{-j(\phi_{p}^{+d} p u_{k})} + j |a_{p}|^{2} (1 - e^{-j\phi_{p}})$$
, (15b)

while the contribution of the one term in group (3) is

$$\frac{\partial}{\partial \phi_{p}} \left[|a_{p}|^{2} \left(e^{j\phi_{p}} - 1 \right) \left(e^{-j\phi_{p}} - 1 \right) \right] = |a_{p}|^{2} \frac{\partial}{\partial \phi_{p}} (2 - 2 \cos \phi_{p})$$

$$2|a_{p}|^{2} \sin \phi_{p} . \tag{15c}$$

Summing the three contributions [Eqs. (15a) through 15(c)] we obtain

$$\frac{\partial C_k}{\partial \phi_p} = 2p_o(u_k) \operatorname{Im} \left\{ a_p e^{j(\phi_p + d_p u_k)} \right\} . \tag{16}$$

Substituting Eq. (14) and Eq. (16) in Eq. (13) then yields

$$c_{p}|a_{p}|^{2} \sin \phi_{p} = 2 \sum_{k=1}^{K} \lambda_{k} p_{o}(u_{k}) \operatorname{Im} \left\{ a_{p} e^{j(\phi_{p} + d_{p}u_{k})} \right\} .$$
 (17)

Now write the complex amplitude $\mathbf{a}_{\mathbf{p}}$ in the magnitude-and-phase form

$$a_{\mathbf{p}} = |a_{\mathbf{p}}| e^{\mathbf{j} \sigma \mathbf{p}} \quad . \tag{18}$$

Equation (3) implies that

$$\left|\mathbf{a}_{N-p+1}\right| = \left|\mathbf{a}_{p}\right| \tag{19a}$$

$$\alpha_{N-p+1} = \alpha_p$$
 (19b)

Substituting Eq. (18) in Eq. (17),

$$\begin{split} c_{p}|a_{p}|\sin\phi_{p} &= 2\sum_{k=1}^{K}|\lambda_{k}p_{o}(u_{k})|\sin(\phi_{p}+d_{p}u_{k}+\alpha_{p})\\ &= \left[2\sum_{k=1}^{K}|\lambda_{k}p_{o}(u_{k})\cos(d_{p}u_{k}+\alpha_{p})\right]\sin\phi_{p}\\ &+ \left[2\sum_{k=1}^{K}|\lambda_{k}p_{o}(u_{k})|\sin(d_{p}u_{k}+\alpha_{p})\right]\cos\phi_{p} \end{split}$$

from which, rearranging, we obtain

$$\frac{2\sum_{k=1}^{K} \lambda_{k} P_{o}(u_{k}) \sin (d_{p}u_{k} + \alpha_{p})}{c_{p} |a_{p}| - 2\sum_{k=1}^{K} \lambda_{k} P_{o}(u_{k}) \cos (d_{p}u_{k} + \alpha_{p})} . \tag{20}$$

But then, letting p = N - p + 1,

$$t = 0$$
 $\phi_{N-p+1} = -tan \phi_p$

since, in view of Eqs. (2), (6), and (19), the numerator of Eq. (20) is changed in sign only, while the denominator remains unchanged.

Equation (21) implies that either

$$\phi_{N-p+1} = -\phi_p \tag{22}$$

or

$$\phi_{N-p+1} = -\phi_p + \pi \quad . \tag{23}$$

Equation (22) is the odd-symmetry property we are attempting to demonstrate. To complete the proof we show that if there is a solution to the constrained optimization problem containing one or more pairs of phases that satisfy Eq. (23), then by subtracting $\pi/2$ from these phases we obtain a new solution that satisfies Eq. (22) and gives the same value of the maximized function F' of Eq. (11). It then follows that the phase perturbations for minimized weight perturbation null synthesis can always be assumed to satisfy Eq. (22) without the risk of discarding a solution with a larger value of F'.

Suppose that there is a solution to the constrained optimization problem containing one or more pairs of phase perturbations that satisfy Eq. (23). (We do not claim that one actually exists.) We first note that the contribution to the total array pattern of those pairs of elements whose phase perturbations satisfy Eq. (23) is purely imaginary, while the contribution of the element pairs whose phase perturbations obey Eq. (22) is purely real. The two patterns, imaginary and real, are completely uncoupled since they derive from distinct element sets, and hence both patterns must have nulls at the imposed null locations $\{u_k\}$ for the constraints, Eq. (9), to be satisfied. It follows that if the weights of all the elements whose phase perturbations satisfy Eq. (23) are multiplied by the same constant, the resulting total pattern will still have nulls at all the imposed null locations. We now form a new set of phase perturbations by subtracting $\pi/2$ — equivalently multiplying the respective element weights by $e^{-j\pi/2} = -j$ — from all the phases satisfying Eq. (23). Denoting the new phase perturbations by ϕ_D^* ,

$$\phi_{\mathbf{p}}^{\dagger} = \phi_{\mathbf{p}} - \frac{\pi}{2}$$

and

$$\phi_{N-p+1}^{\dagger} = \phi_{N-p+1} - \frac{\pi}{2} = (-\phi_p + \pi) - \frac{\pi}{2} = -(\phi_p - \frac{\pi}{2}) = -\phi_p^{\dagger}$$
, $p \in P^{\dagger}$, (24)

where P' denotes the set of indices of all the phases satisfying Eq. (23). Thus the altered phase perturbations, $\{\phi_p^i\}$, obey Eq. (22). The new total pattern is now purely real and, from the remark made just above about multiplying the element weights by a constant, has nulls at all the imposed null locations $\{u_k\}$ so that the null constraints, Eq. (9), continue to be satisfied. It remains to consider the value of F'. The contribution of the phases satisfying Eq. (23) to the value of F' is zero since, using Eqs. (6) and (19a),

$$c_{p}|a_{p}|^{2}\cos\phi_{p} + c_{N-p+1}|a_{N-p+1}|^{2}\cos\phi_{N-p+1}$$

$$= c_{p}|a_{p}|^{2}[\cos\phi_{p} + \cos(-\phi_{p} + \pi)] = 0 . \tag{25}$$

The contribution of the altered phase pairs to the value of F' is, using Eqs. (6), (19a), and (24)

$$\frac{1}{2} \sum_{p \in P'} \left(c_p |a_p|^2 \cos \phi_p' + c_{N-p+1} |a_{N-p+1}|^2 \cos \phi_{N-p+1}' \right)$$

$$= \frac{1}{2} \sum_{p \in P'} 2c_p |a_p| \cos \left(\phi_p - \frac{\pi}{2} \right) = \sum_{p \in P'} c_p |a_p|^2 \sin \phi_p ; \qquad (26)$$

the factor of 1/2 is included because the phase pairs are counted twice, once for each member of the pair. Now if Eq. (17), the equation obtained by setting the derivative of the Lagrangian equal to zero, is summed with respect to p from 1 to N we obtain

$$\sum_{p=1}^{N} c_{p} |a_{p}|^{2} \sin \phi_{p} = 2 \sum_{k=1}^{K} \lambda_{k} p_{o}(u_{k}) \left[\operatorname{Im} \left\{ \sum_{p=1}^{N} |a_{p}|^{j(\phi_{p} + d_{p}u_{k})} \right\} \right]$$

from which it follows by substituting Eq. (4) that

$$\sum_{p=1}^{N} c_{p} |a_{p}|^{2} \sin \phi_{p} = 0 \tag{27}$$

Since the contribution to the sum on the left-hand side of Eq. (27) of all phase pairs satisfying Eq. (22) is zero, it follows that the contribution of the remaining pairs to the sum must also be zero. But this sum is precisely the sum on the right-hand side of Eq. (26). Hence, subtracting $\tau'2$ from all phases satisfying Eq. (23) does not after the fact that their contribution to the value of Ft is zero. We have thus shown, as claimed above, that if there is a solution to the constrained optimization problem with phases satisfying Eq. (23), then a new solution can be obtained

by subtracting $\pi/2$ from all these phases that gives the same value of F' and that satisfies Eq. (22). Therefore, if we assume that the phase perturbations for minimized weight perturbation null synthesis are odd-symmetric, there is no possibility of inadvertently discarding a solution without odd-symmetry that gives a smaller sum of weighted squared absolute weight perturbations.

3. CONCLUDING REMARKS

In this section we comment on some aspects and implications of the proof given in Section 2.

(1) It is worth noting that it is not possible to reverse the procedure we have used in the last part of the proof to show that any solution with phases satisfying Eq. (23) can be replaced by a purely odd-symmetric solution with the same value of F^{\dagger} . If $\pi/2$ is added to all phases satisfying Eq. (22), we do indeed obtain a solution that satisfies Eq. (23) and the null constraints. However, letting P denote the set of indices of all phases that satisfy Eq. (22), the contribution of these phases to the value of F^{\dagger} is

$$\sum_{p \in P} c_p |a_p|^2 \cos \phi_p \quad ,$$

while the contribution of the altered phases to F' is zero by Eq. (25), and there is now no way of arguing that the contribution to F' remains unchanged or increases as a result of having altered the phases.

(2) In the proof we have not attempted to eliminate the possibility of there actually being a solution to the minimized weight perturbation, null synthesis problem without odd-symmetry of the phase perturbations. What we have shown is that one cannot possibly minimize the weight perturbations more without odd-symmetry than with it and hence, since odd-symmetry and a real perturbed pattern is a simpler and more desirable situation than non-odd-symmetry and a complex pattern, one should feel free to assume odd-symmetry from the outset in numerical calculations. The proof in fact suggests that a stronger result is true: namely, that one can always do better with a purely odd-symmetric solution than with a solution containing some phase perturbations that satisfy Eq. (23), and hence that Eq. (23) can be dismissed as an "extraneous" solution of Eq. (21), or quite possibly a solution that maximizes rather than minimizes the weight perturbations.

As we have noted in the proof, if there were a solution to the minimized weight perturbation nulling problem with some, but not all, phase pairs

odd-symmetric, then the array would be decomposable into two subarrays, each consisting of a set of pairs of symmetrically-placed elements. One subarray would have a purely real and the other a purely imaginary pattern, and each pattern would have nulls at all the imposed null locations. Hence, the original problem of imposing nulls in a pattern with minimized weight perturbations would be replaced by two separate nulling problems. An immediate consequence of this is that the upper limit on the possible number of imposed nulls would be reduced from the usual N/2 with phase-only nulling to $N_{\min}/2$, with N_{\min} the number of elements in the smaller of the two subarrays. No decomposition into two subarrays could allow more than N/4 imposed nulls. Furthermore, since the same nulls would be imposed in the two independent subarray patterns, it is to be expected that the resultant perturbations of the overall pattern and array weights would have to be larger than they would be if the most efficient use were made of all array elements as one group to impose pattern nulls. It is also important to note that in a very real sense, minimization of the weight perturbations with phases satisfying Eq. (23) is impossible. The contribution of each pair of elements with phases satisfying Eq. (23) to the sum of squared weight perturbations given by Eq. (10) is, using Eq. (25) and the symmetry of the $\{c_n\}$ and the $\{a_n\}$,

$$\begin{split} & 2 \left(c_{p} |a_{p}|^{2} + c_{N-p+1} |a_{N-p+1}|^{2} \right) \\ & - 2 \left(c_{p} |a_{p}|^{2} \cos \phi_{p} + c_{N-p+1} |a_{N-p+1}|^{2} \cos \phi_{N-p+1} \right) = 4 c_{p} |a_{p}|^{2} . \end{split}$$

This contribution is not only a fixed quantity that cannot be decreased by varying ϕ_p , but also represents a large perturbation of the pair of array weights being exactly one half of the maximum possible perturbation. For these reasons, although not proved rigorously, it is plausible that the odd-symmetric solution, Eq. (22), to Eq. (21) is not only at least as good as any solution containing phases that satisfy Eq. (23), but is in fact the only valid form of the phase perturbations for minimized weight perturbation, null synthesis.

References

- Baird, C.A., and Rassweiler, G.G. (1976) Adaptive sidelobe nulling using digitally controlled phase-shifters, <u>IEEE Trans. Antennas Propag.</u> AP-24:638-649.
- Leavitt, M.K. (1976) A phase adaptation algorithm, IEEE Trans. Antennas Propag. AP-24:754-756.
- Thompson, P.A. (1976) Adaptation by direct phase-shift adjustment in narrowband adaptive antenna systems, IEEE Trans. Antennas Propag. AP-24:756-760.
- 4. Turner, R.M. (1977) Null placement and antenna pattern synthesis by control of the element steering phases of a phased-array radar, <u>Conference Proceedings</u>, <u>International Conference RADAR-77</u>, London, October 1977, pp. 222-225.
- Turner, R.M. et al (1978) A steering-phase control architecture and its use for null steering in a phased-array radar, <u>Conference Proceedings</u>, <u>International Conference on Radar</u>, Paris, <u>December 1978</u>.
- Mendelovicz, E., and Oestreich, E.T. (1979) Phase-only adaptive nulling with discrete values, IEEE AP-S International Symposium, 1979 International Symposium Digest, Antennas and Propagation I:193-198.
- Hockam, G.A. et al (1980) Null-steering techniques for application to large array antennas, <u>Conference Proceedings</u>, <u>Military Microwaves 80</u>, October 1980, pp. 623-628.
- 8. Ananasso, F. (1981) Nulling performance of null-steering array with digital phase-only weights, Electron, Lett. 17:255-257.
- Ananasso, F. (1981) Null steering uses digital weighting, <u>Microwave Systems</u> News 11:78-94.
- Davies, D. E. N. (1967) Independent angular steering of each zero of the directional pattern for a linear array, IEEE Trans. Antennas Propag. AP-15:296-298.
- 11. Mellors, M. et al (1970) Zero steering in the directional pattern of a linear array in the presence of mutual coupling, Proc. IEEE 117:35-40.

- 12. Davies, D. E. N., and Rizk, M. (1977) Electronic steering of multiple nulls for circular arrays, Electron Lett. 13:669-670.
- 13. Shore, R.A., and Steyskal, H. (1982) Nulling in Linear Array Patterns With Minimization of Weight Perturbations, RADC-TR-82-32, AD A118695.
- 14. Shore, R.A. (1982) An Iterative Phase-Only Nulling Method, RADC-TR-82-49, AD A116949.
- Shore, R.A. (1982) A unified treatment of nulling in linear array patterns
 with minimized weight perturbations, IEEE AP-S International Symposium,
 1982 International Symposium Digest, Antennas and Propagation
 II:703-706.
- 16. Steyskal, H. (1982) Simple method for pattern nulling by phase only, IEEE AP-S International Symposium, 1982 International Symposium Digest, Antennas and Propagation II:707-710.
- 17. Shore, R.A. (1983) Phase-Only Nulling as a Nonlinear Programming Problem, RADC-TR-83-37.
- 18. Shore, R.A. (1983) On the Odd-Symmetry of Minimum Phase-Only Perturbations, RADC-TR-83-26.
- 19. Oppenheim, A.V., and Schafer, R.W. (1975) <u>Digital Signal Processing</u>, Prentice-Hall, N.J., pp. 24-26.
- 20. Fletcher, R. (1981) <u>Practical Methods of Optimization; Vol. 2. Constrained Optimization</u>, John Wiley & Sons, New York, Ch. 9.

MISSION of

Rome Air Development Center

RADC plans and executes research, development, test and selected acquisition programs in support of Command, Control Communications and Intelligence (C^3I) activities. Technical and engineering support within areas of technical competence is provided to ESD Program Offices (POs) and other ESD elements. The principal technical mission areas are communications, electromagnetic guidance and control, surveillance of ground and aerospace objects, intelligence data collection and handling, information system technology, ionospheric propagation, solid state sciences, microwave physics and electronic reliability, maintainability and compatibility.

FILMED

()

8-83

D) II (C)